

Question A3, 1997:

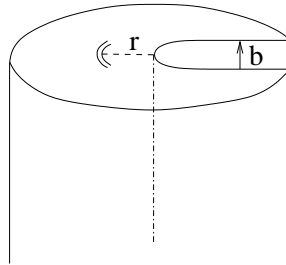
Screw dislocation: dislocation for which the Burgers vector is parallel to the dislocation line (line marking the boundary between slipped and unslipped regions of the crystal)

Edge dislocation: dislocation for which the Burgers vector is normal to the dislocation line.

Burgers vector: vector describing the magnitude and direction of the displacement due to the passage of a dislocation.

Slip system: the combination of slip plane (hkl) and slip direction [UVW] lying in this plane.

Energy of a screw dislocation:



we consider the cylinder formed by the material between r and $r + dr$, its shear strain is:

$$\gamma = \frac{b}{2\pi r}$$

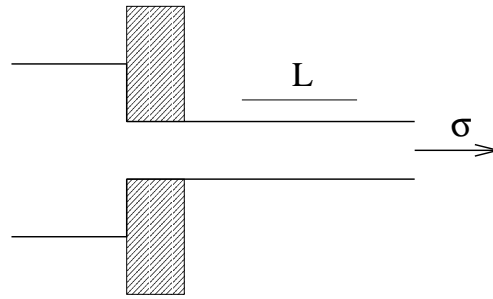
Given its volume $2\pi r L dr$ where L is the length of the dislocation, the strain energy in this cylinder is:

$$\frac{1}{2} G \gamma^2 2\pi r L dr$$

by substituting γ and integrating between r_0 , lower limit where the strain is no longer elastic, and R , which can, for example, be half the distance to the next dislocation, the energy per unit length of dislocation is:

$$U = \frac{Gb^2}{4\pi} \int_{r_0}^R \frac{dr}{r} + \text{core energy}$$

Cold drawing of Al:



Consider a length L of the Al after drawing. The work required to produce it is obviously:

$$\sigma AL$$

where A is the cross section of the wire. The increase in dislocation density ΔN is associated with an energy increase given by:

$$\Delta N \times AL \times \frac{1}{2}Gb^2$$

identifying this quantity to 1% of the work done leads to:

$$\Delta N = \frac{0.02\sigma}{Gb^2}$$

Al being a fcc metal, $b = a/\sqrt{2}$. ΔN can then be estimated:

$$\Delta N \sim 1.7 \times 10^{14} \text{m}^{-3}$$

The rise in temperature is obtained by identifying:

$$0.99\sigma = C_v \Delta T$$

giving:

$$\Delta T \sim \frac{\sigma}{C_v} \sim 7\text{K}$$

Therefore the temperature rise is not expected to be a limiting factor. The mechanical deterioration of the wire is more likely to be (must keep σ below the universal tensile strength).